

# *NAMIBIA UNIVERSITY*

OF SCIENCE AND TECHNOLOGY

# **FACULTY OF ENGINEERING AND THE BUILT ENVIRONMENT**

## DEPARTMENT OF CIVIL, MINING AND PROCESS ENGINEERING

QUALIFICATION: BACHELOR OF ENGINEERING IN METALLURGY				
QUALIFICATION CODE: 08BMET	LEVEL: 8			
COURSE CODE: HMY720S	COURSE NAME: HYDROMETALLURGY 324			
SESSION: NOVEMBER 2022	PAPER: 1			
DURATION: 90 MINUTES	MARKS: 50			

	SECOND OPPORTUNITY QUESTION PAPER	
EXAMINER(S)	Prof D Groot	
MODERATOR:	Dr T Coetsee, University of Pretoria	

IN	STRUCTIONS
1.	Answer all questions.
2.	Read all the questions carefully before answering.
3.	Marks for each questions are indicated at the end of each question.
4.	Please ensure that your writing is legible, neat and presentable.

### PERMISSIBLE MATERIALS

- 1. Examination paper.
- 2. Scientific calculator, non-programmable

THIS QUESTION PAPER CONSISTS OF 5 PAGES (Including this front page)



#### Question 1

Consider a Sherritt-type cobalt refinery as shown below.

- (a) Explain the chemical principles used to separate nickel from cobalt in this flowsheet, and why it is necessary as the hydrogen reduction step is selective. [5]
- (b) Draw a modified flowsheet to recover the cobalt as cathode.

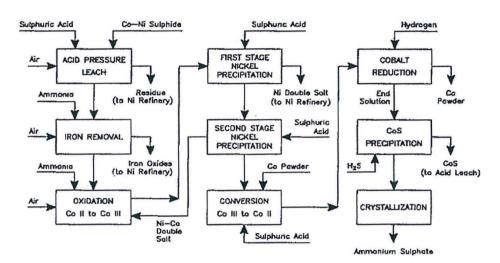


Figure 10. Sherritt Cobalt Refinery Flowsheet

#### Question 2

The 4f (lanthanides) and 5f (actinides) elements differ considerably in their chemistries. The chemistry of both periods of elements also differs much from the transition metals.

- (a) Discuss how the 4f and 5f elements generally differ in terms of their coordination chemistry.
  - [3]

[3]

(b) Discuss how the ability of the 5f elements to form unusual complex ions (as compared to transition metals) is used in the extraction of uranium from its ores. [5]

### Question 3

Discuss the factors that affect the morphology (i.e. what the deposit looks like) of copper electrodeposits.

[8]

#### Question 4

Nickel ores are found as sulfides and as laterites.

(a) Describe the operation of the Moa Bay process for laterite ores.

- [5]
- (b) Briefly discuss how the environmental impact of this plant could be reduced.



#### Question 5

Consider a typical hydrometallurgical plant.

- (a) Explain why a series of stirred tank reactors are used, instead of a single, large reactor with the same retention time. [3]
- (b) Would a number of parallel stirred tank reactors (same number, same retention time) have the efficiency as a series? Explain your answer. [2]
- (c) Explain how a stirred tank reactor on a plant differs from a CSTR. [3]
- (d) Discuss how the difference in performance between a real reactor and a CSTR can be dealt with during plant design. [6]

### **Question 6**

You wish to model the dissolution kinetics of calcium oxide particles in a 0.01 mol/l solution of hydrochloric acid. The particles are +10 -72 micron. A number of experiments are done at various temperatures and stirring rates. It is found that the measured rate is fairly insensitive to the temperature, but varies greatly with stirring.

Calculate the expected time for the dissolution of all particles.

[5]

Given: density of calcium oxide:  $3.34 \text{ g/cm}^3$ ; diffusion coefficient:  $7.93 \times 10^{-4} \text{ cm}^2/\text{s}$  at 20 deg; solubility of the reaction product is 74.5 g/100 ml (20 °C).

## Given information

See following pages (2).



Table 25.1 Conversion-Time Expressions for Various Shapes of Particles, Shrinking-Core Model

		Film Diffusion Controls		Ash Diffusion Controls		Reaction Controls	
Constant Size Particles	Flat plate $X_{\rm B} = 1 - \frac{1}{L}$ $L = \text{half thickness}$	$\frac{t}{\tau} = X_{\rm B}$		$\frac{t}{\tau} = X_{\rm B}^2$		$\frac{t}{\tau} = X_{\rm B}$	
		$\tau = \frac{\rho_{\rm B}L}{bk_{\rm g}C_{\rm Ag}}$		$\tau = \frac{\rho_{\rm B} L^2}{2b \mathcal{D}_{\rm e} C_{\rm Ag}}$		$\tau = \frac{\rho_{\rm B}L}{bk''C_{\rm Ag}}$	************
	Cylinder	$\frac{t}{\tau} = X_{\rm B}$		$\frac{t}{\tau} = X_{\rm B} + (1 - X_{\rm B}) \ln(1 - X_{\rm B})$		$\frac{t}{\tau} = 1 - (1 - X_{\rm B})^{1/2}$	
	$X_{\rm B} = 1 - \left(\frac{r_{\rm c}}{R}\right)^2$	$\tau = \frac{\rho_{\rm B}R}{2bk_{\rm g}C_{\rm Ag}}$		$\tau = \frac{\rho_{\rm B} R^2}{4b \mathcal{D}_{\rm e} C_{\rm Ag}}$		$\tau = \frac{\rho_{\rm B}R}{bk''C_{\rm Ag}}$	
	Sphere	$\frac{t}{\tau} = X_{\rm B}$	(11)	$\frac{t}{\tau} = 1 - 3(1 - X_{\rm B})^{2/3} + 2(1 - X_{\rm B})$	(18)	$\frac{t}{\tau} = 1 - (1 - X_{\rm B})^{1/3}$	(23)
	$X_{\rm B} = 1 - \left(\frac{r_{\rm c}}{R}\right)^3$	$\tau = \frac{\rho_{\rm B}R}{3bk_{\rm g}C_{\rm Ag}}$	(10)	$\tau = \frac{\rho_{\rm B} R^2}{6b \mathcal{D}_e C_{\rm Ag}}$	(17)	$\tau = \frac{\rho_{\rm B}R}{bk''C_{\rm Ag}}$	(22)
Shrinking Sphere	Small particle Stokes regime	$\frac{t}{\tau} = 1 - (1 - X_{\rm B})^{2/3}$	(30)	Net and Parkin		$\frac{t}{\tau} = 1 - (1 - X_{\rm B})^{1/3}$	
		$\tau = \frac{\rho_{\rm B} R_0^2}{2b \mathcal{D} C_{\rm Ag}}$	(29)	Not applicable		$\tau = \frac{\rho_{\rm B} R_0}{b k'' C_{\rm Ag}}$	
	Large particle $(u = constant)$	$\frac{t}{\tau} = 1 - (1 - X_{\rm B})^{1/2}$	(31)	Not applicable		$\frac{t}{\tau} = 1 - (1 - X_{\rm B})^{1/3}$	
		$\tau = (\text{const}) \frac{R_0^{3/2}}{C_{\text{Ag}}}$		Not applicable		$\tau = \frac{\rho_{\rm B}R}{bk''C_{\rm Ag}}$	



